

DYNAMIC MODELING OF BRAKE IN POWER-SPLIT DHT AND PRESSURE TRACKING CONTROL WITH SLIDING MODE VARIABLE STRUCTURE METHOD

Zhiguo Zhao^{1)*}, Mengna Li¹⁾, Chen Wang^{1, 2)}, Lanxing Jiang¹⁾ and Maoyao Wang¹⁾

¹⁾School of Automotive Studies, Tongji University, Shanghai 201804, China

²⁾System Control Department, Corun CHS Technology Co., Ltd., No. 2880 Wanfeng Road, Jinshan District, Shanghai 201501, China

(Received 26 February 2018; Revised 28 May 2018; Accepted 13 November 2018)

ABSTRACT—Since the mode transition performance of power-split DHT (Dedicated Hybrid Transmission) are directly influenced by torque dynamic characteristic of the brake, the brake pressure should be controlled accurately. In this paper, a dynamic model of brake and its pressure regulating system are established by considering system nonlinear characteristics and input disturbances, and a sliding mode variable structure controller is developed to track the brake pressure. First, the operation principle of DHT's pressure regulating system is introduced. Second, the dynamic models of solenoid proportional pressure valve, electromagnetic direction switching valve and brake are established with AMESim parametric plant model. Furthermore, a sliding mode variable structure controller for tracking pressure is designed based on MATLAB/Simulink. Finally, the AMESim parametric plant model is validated by measurements, and the proposed controller are verified by AMESim and Simulink co-simulation. The results show that the system dynamics can be well characterized by the AMESim parametric plant model. The target pressure can be tracked rapidly and accurately by using sliding mode variable structure controller and the controller has better robustness.

KEY WORDS : Dedicated Hybrid Transmission (DHT), Hydraulic system, Dynamic modeling, Sliding mode variable structure

NOMENCLATURE

A_{ex3} : flow area of exhaust port
 A_{in3} : flow area of supply port
 A_{fb3o} : flow area of the orifice in feedback chamber
 A_{fb} : effective action area of feedback chamber
 A_p : effective piston action area
 A_{po} : orifice area
 C_d : flow coefficient
 c_m, c_s : constant coefficients
 c_p : piston equivalent damping coefficient
 c_{s3} : equivalent damp coefficient of valve spool
 d_{fb3o} : diameter of orifice in feedback chamber
 d_{po} : diameter of orifice
 d_p : diameters of piston chamber
 d_{s3l}, d_{s3r} : diameter of left and right side of valve spool in feedback chamber
 d_r : diameter of piston rod
 F_{s3} : solenoid force
 F_{drag} : resistance force of seal rings
 k_m, k_s : constant coefficients
 m_p : piston mass
 m_{s3} : mass of valve spool

P_{sup3} : supply port pressure
 P_{out3} : output port pressure
 P_{fb3} : feedback chamber pressure
 P_p : oil pressure in brake chamber
 Q_{in3} : supply port flow
 Q_{out3} : output port flow
 Q_{fb3} : feedback chamber flow
 Q_{ex3} : exhaust port flow
 Q_{imp} : flow of the supply port of brake chamber
 Q_{exp} : flow of the exhaust port of brake chamber
 V_3 : volume of the main chamber
 V_{fb3} : volume of the feedback chamber
 V_p : initial volume of clutch chamber
 x_{s3} : displacement of valve spool
 x_{s30} : initial displacement of valve spool
 x_p : piston displacement
 x_{p0} : initial piston displacement
 α : damping coefficient of seal rings in piston chamber
 β : volume modulus
 ρ : oil density

1. INTRODUCTION

As one of the typical full and plug-in hybrid systems, power-split DHT utilizes planetary gear train to integrate or

*Corresponding author. e-mail: zhiguo Zhao@tongji.edu.cn